2.2 MITIGATING SYSTEMS CORNERSTONE

- 2 The objective of this cornerstone is to monitor the availability, reliability, and capability of
- 3 systems that mitigate the effects of initiating events to prevent core damage. Licensees reduce
- 4 the likelihood of reactor accidents by maintaining the availability and reliability of mitigating
- 5 systems. Mitigating systems include those systems associated with safety injection, decay heat
- 6 removal, and their support systems, such as emergency ac power. This cornerstone includes
- 7 mitigating systems that respond to both operating and shutdown events.

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- 9 Some aspects of mitigating system performance cannot be adequately reflected or are
- 10 specifically excluded from the performance indicators in this cornerstone. These aspects include
- 11 performance of structures, systems, and components (SSCs) specifically excluded from the
- 12 performance indicators, the effect of common cause failure, and the performance of certain plant
- 13 specific systems. These aspects of licensee performance will be addressed through the NRC
- 14 inspection program.
- 15 There are two sets of indicators in this cornerstone:

16

- 17 Mitigating System Performance Index
 - Safety System Functional Failures

18 19 20

MITIGATING SYSTEM PERFORMANCE INDEX

21 **Purpose**

- 22 The purpose of the mitigating system performance index is to monitor the risk impact of changes
- 23 in performance of selected systems. It is comprised of two elements - system unavailability and
- 24 system unreliability.

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Indicator Definition

27 Mitigating system performance index (MSPI) is the sum of changes in a simplified core damage 28

frequency evaluation resulting from changes in train unavailability and train unreliability relative to baseline values.

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Train unavailability is the ratio of the hours the train was unavailable to perform its risksignificant functions due to preventive or corrective maintenance or test during the previous 12 quarters while critical to the number of critical hours during the previous 12 quarters. (Fault

exposure hours are not included; unavailable hours are counted only for the time required to

recover the train's risk-significant functions.)

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Train unreliability is the probability that the train would not perform its risk-significant functions when called upon during the previous 12 quarters.

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Baseline values are the values for unavailability and unreliability against which current changes in unavailability and unreliability are measured. See Appendix F for further details.

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Th	e MSPI is calculated separately for each of the following five systems for each reactor type.
BV	VRs
•	emergency AC power system
•	high pressure injection systems (high pressure coolant injection, high pressure core spray, or
	feedwater coolant injection)
•	heat removal systems (reactor core isolation cooling)
•	residual heat removal system
	cooling water support system (includes risk significant direct cooling functions provided by service water and component cooling water or their cooling water equivalents for the above four monitored systems)
PV	VRs
•	emergency AC power system
•	high pressure safety injection system
•	auxiliary feedwater system
•	residual heat removal system
•	cooling water support system (includes risk significant direct cooling functions provided by
	service water and component cooling water or their cooling water equivalents for the above
	four monitored systems)
Da	ta Reporting Elements
Th	e following data elements are reported for each system
•	Unavailability Index (UAI) due to unavailability for each monitored system
•	Unreliability Index (URI) due to unreliability for each monitored system
	Official interview (ON) due to differ ability for each monitored system
Du	ring the pilot, the following additional data elements are reported monthly for each system
•	critical hours
•	unavailable hours by train
•	the following unreliability data elements defined in Appendix F
	\triangleright n _d = total number of failures on demand during the previous 12 quarters
	d = total number of demands during the previous 12 quarters
	n_r = total number of failures to run during the previous 12 quarters
	 t = total number of run hours during the previous 12 quarters T = mission time based on plant-risk model assumptions
	1 – Illission time based on plant risk model assumptions
Ca	<u>llculation</u>
	e MSPI for each system is the sum of the UAI due to unavailability for the system plus URI e to unreliability for the system during the previous twelve quarters.
uu	to differentiality for the system during the previous twerve quarters.
MS	SPI = UAI + URI.

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See Appendix F for the calculational methodology for UAI due to system unavailability and URI due to system unreliability.

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Definition of Terms

A train consists of a group of components that together provide the risk significant functions of
 the system as explained in the additional guidance for specific mitigating systems. Fulfilling the
 risk significant function of the system may require one or more trains of a system to operate
 simultaneously. The number of trains in a system is determined as follows:

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• for systems that provide cooling of fluids, the number of trains is determined by the number of parallel heat exchangers, or the number of parallel pumps, or the minimum number of parallel flow paths, whichever is fewer.

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• for emergency AC power systems the number of trains is the number of class 1E emergency (diesel, gas turbine, or hydroelectric) generators at the station that are installed to power shutdown loads in the event of a loss of off-site power (This does not include the diesel generator dedicated to the BWR HPCS system, which is included in the scope of the HPCS system).

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Risk Significant Functions: those at power functions of risk-significant SSCs as defined in NUMARC 93-01 (revision 3), Section 9.3, as endorsed by the NRC in Regulatory Guide 1.160 for meeting the requirements of the maintenance rule.

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Success criteria are the plant specific values of parameters that identify the capability of the train/system that is required to meet the risk-significant function. Default values of parameters are the plant's design bases values unless other values are modeled in the PRA.

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Clarifying Notes

Documentation

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- It is expected that each licensee will have identified the system boundaries, active components, risk significant functions and success criteria necessary to report this performance indicator.
- This information shall be readily available for NRC inspection on site. Additionally, plantspecific information used in Appendix F should also be readily available for inspection.

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Success Criteria

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- Typical plant specific performance factors that can be used to identify the capability of the train to meet the risk-significant functions include, but are not limited to:
- 41 Actuation
 - o Time
- 43 o Auto/manual
- o Multiple or sequential

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1	Success requirements
2	 Numbers of components or trains
3	o Flows
4	o Pressures
5	 Heat exchange rates
6	 Temperatures
7	Other mission requirements
8	o Run time
9	 State/configuration changes during mission
10	Accident environment from internal events
11	o Pressure, temperature, humidity
12	 Operational factors
13	o Procedures
14	o Human actions
15	o Training
16	 Available externalities (e.g., power supplies, special equipment, etc.)
17	O Available externations (e.g., power supplies, special equipment, etc.)
18	Monitored Systems
	Monitored Systems
19	Crystams have been considerly selected for this indicator based on their immertance in preventing
20	Systems have been generically selected for this indicator based on their importance in preventing
21	reactor core damage. The systems include the principal systems needed for maintaining reactor
22	coolant inventory following a loss of coolant accident, for decay heat removal following a
23	reactor trip or loss of main feedwater, and for providing emergency AC power following a loss
24	of plant off-site power. One risk-significant support function (support cooling system) is also
25	monitored. The support cooling system monitors the risk significant cooling functions provided
26	by service water and component cooling water, or their direct cooling water equivalents, for the
27	four front-line monitored systems. No support systems are to be cascaded onto the monitored
28	systems, e.g., HVAC room coolers, DC power, instrument air, etc.
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30	<u>Diverse Systems</u>
31	
32	Except as specifically stated in the indicator definition and reporting guidance, no credit is given
33	for the achievement of a risk significant function by an unmonitored system in determining
34	unavailability or unreliability of the monitored systems.
35	
36	Common Components
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38	Some components in a system may be common to more than one train, in which case the effect
39	of the performance (unavailable hours) of a common component is included in all affected trains.
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41	
42	System or equipment realignments and activities
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44	Trains are generally considered to be available during periodic system or equipment
45	realignments to swap components or flow paths as part of normal operations. Evolutions or

surveillance tests that result in less than 15 minutes of unavailable hours per train at a time

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should not be counted as unavailable hours. The intent is to minimize unnecessary burden of data collection, documentation, and verification. Licensees should compile a list of surveillances/evolutions that meet this criterion and have it available for inspector review.

If a licensee is required to take a component out of service for evaluation and corrective actions (for example, related to a Part 21 Notification), the unavailable hours must be included.

Treatment of Degraded Conditions

If a degraded condition results in the failure to meet an established success criterion, unavailable hours must be included for the time required to recover the train's risk-significant function(s). If an active component, as defined in this guidance, is degraded such that it cannot meet its risksignificant function, a demand and a demand failure are also counted. If subsequent analysis identifies additional margin for the success criterion, future unavailable hours for degraded conditions may be determined based on the new criterion. However, unavailability must be based on the success criteria of record at the time the degraded condition is discovered. If the degraded condition is not addressed by any of the pre-defined success criteria, an engineering evaluation to determine the impact of the degraded condition on the risk-significant function(s) should be completed and documented. The use of component failure analysis, circuit analysis, or event investigations is acceptable. Engineering judgment may be used in conjunction with analytical techniques to determine the impact of the degraded condition on the risk-significant function. The engineering evaluation should be completed as soon as practicable. If it cannot be completed in time to support submission of the PI report for the current quarter, the comment field shall note that an evaluation is pending. The evaluation must be completed in time to accurately account for unavailability/unreliability in the next quarterly report. Exceptions to this guidance are expected to be rare and will be treated on a case-by-case basis. Licensees should identify these situations to the resident inspector.

Failures on Demand

Failures of active components (see Appendix F) on demand, either actual or test, while critical, are included in unreliability. Failures on demand while non-critical must be evaluated to determine whether the failure would have resulted in the train not being able to perform its risk-significant at power functions, and hence be included in unreliability. Unavailable hours are included only for the time required to recover the train's risk-significant functions and only when the reactor is critical.

Discovered Conditions

Discovered conditions that render an active component incapable of performing its risk-significant functions are included in unreliability as a demand and a failure. Unavailable hours are counted only for the time required to recover the train's risk-significant functions and only when the reactor is critical. The ROP inspection process would be used to determine the significance of discovered conditions that rendered a train incapable of performing its risk-significant function, but were not active component conditions (for example, a shut manual suction valve).

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<u>Demand failures or discovered conditions that are not capable of being discovered during normal</u> surveillance tests

These failures or conditions are usually of longer exposure time. Since they have not been tested on a regular basis, it is inappropriate to include them in the performance index statistics. These failures or conditions are subject to evaluation through the inspection process. Examples of this type are failures due to pressure locking/thermal binding of isolation valves, blockages in lines not regularly tested, or inadequate component sizing/settings under accident conditions (not under normal test conditions). While not included in the calculation of the index, they should be reported in the comment field of the PI data submittal.

Credit for Operator Recovery Actions to Restore the Risk-Significant Function

1. During testing or operational alignment:

Unavailability of a risk-significant function during testing or operational alignment need not be included if the test configuration is automatically overridden by a valid starting signal, or the function can be promptly restored in time to meet the PRA risk success criteria either by an operator in the control room or by a designated operator¹ stationed locally for that purpose. Restoration actions must be contained in a written procedure², must be uncomplicated (*a single action or a few simple actions*), and must not require diagnosis or repair. Credit for a designated local operator can be taken only if (s)he is positioned at the proper location throughout the duration of the test for the purpose of restoration of the train should a valid demand occur. The intent of this paragraph is to allow licensees to take credit for restoration actions that are virtually certain to be successful (i.e., probability nearly equal to 1) during accident conditions.

The individual performing the restoration function can be the person conducting the test and must be in communication with the control room. Credit can also be taken for an operator in the main control room provided (s)he is in close proximity to restore the equipment when needed. Normal staffing for the test may satisfy the requirement for a dedicated operator, depending on work assignments. In all cases, the staffing must be considered in advance and an operator identified to perform the restoration actions independent of other control room actions that may be required.

Under stressful, chaotic conditions, otherwise simple multiple actions may not be accomplished with the virtual certainty called for by the guidance (e.g., lifting test leads and landing wires; or clearing tags). In addition, some manual operations of systems designed to operate automatically, such as manually controlling HPCI turbine to establish and control

 $^{^{\}scriptscriptstyle 1}$ Operator in this circumstance refers to any plant personnel qualified and designated to perform the restoration function.

² Including restoration steps in an approved test procedure.

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injection flow, are not virtually certain to be successful. These situations should be resolved on a case-by-case basis through the FAQ process.

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2. During Maintenance

Unavailability of a risk-significant function during maintenance need not be included if the risk-significant function can be promptly restored in time to meet the PRA success criteria either by an operator in the control room or by a designated operator³ stationed locally for that purpose. Restoration actions must be contained in a written procedure⁴, must be uncomplicated (a single action or a few simple actions), and must not require diagnosis or repair. Credit for a designated local operator can be taken only if (s)he is positioned at a proper location throughout the duration of the maintenance activity for the purpose of restoration of the train should a valid demand occur. The intent of this paragraph is to allow licensees to take credit for restoration of risk-significant functions that are virtually certain to be successful (i.e., probability nearly equal to 1). The individual performing the restoration function can be the person performing the maintenance and must be in communication with the control room. Credit can also be taken for an operator in the main control room provided (s)he is in close proximity to restore the equipment when needed. Under stressful chaotic conditions otherwise simple multiple actions may not be accomplished with the virtual certainty called for by the guidance (e.g., lifting test leads and landing wires, or clearing tags). These situations should be resolved on a case-by-case basis through the FAQ process.

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Short Duration Unavailability

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Unavailable periods of less than 15 minutes for any cause do not need to be included in the performance indicator. The intent is to minimize unnecessary burden of data collection, documentation, and verification.

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Swing trains and components shared between units

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Swing trains/components are trains/components that can be aligned to any unit. To be credited as such, their swing capability should be modeled in the PRA to provide an appropriate Fussel-Vessely value.

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Maintenance Trains and Installed Spares

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Some power plants have systems with extra trains to allow preventive maintenance to be carried out with the unit at power without impacting the risk-significant function of the system. That is, one of the remaining trains may fail, but the system can still perform its risk significant function.

³ Operator in this circumstance refers to any plant personnel qualified and designated to perform the restoration function.

⁴ Including restoration steps in an approved test procedure.

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1 2 3	To be a maintenance train, a train must not be needed to perform the system's risk significant function.
4 5 6 7 8	An "installed spare" is a component (or set of components) that is used as a replacement for other equipment to allow for the removal of equipment from service for preventive or corrective maintenance without impacting the risk-significant function of the system. To be an "installed spare," a component must not be needed for the system to perform the risk significant function.
9 10 11 12	Unavailability and unreliability are monitored for an installed spare or maintenance train if it is modeled in the plant PRA. If they are substituted for a primary train/component, the primary becomes the spare.
13 14 15 16 17	If a maintenance train or installed spare are not modeled in the plant PRA, unavailability and unreliability are monitored only when they are substituted for a primary train/component. Unavailability and unreliability are not monitored for a component/train when that component/train has been replaced by an installed spare or maintenance train that is not modeled in the plant PRA.
19	Use of Plant-Specific PRA and SPAR Models
20 21 22 23	The MSPI is an approximation using some information from a plant's actual PRA and is intended as an indicator of system performance. Plant-specific PRAs and SPAR models cannot be used to question the outcome of the PIs computed in accordance with this guideline.
24 25	Maintenance Rule Performance Monitoring
26 27 28	It is the intent that NUMARC 93-01 be revised to require consistent unavailability and unreliability data gathering as required by this guideline.
29 30	ADDITIONAL GUIDANCE FOR SPECIFIC SYSTEMS
31	Emergency AC Power Systems
32	<u>Scope</u>
33 34 35 36 37	The emergency AC power system is typically comprised of two or more independent emergency generators that provide AC power to class 1E buses following a loss of off-site power. The emergency generator dedicated to providing AC power to the high pressure core spray system in BWRs is not within the scope of emergency AC power.
38 39 40 41	The electrical circuit breaker(s) that connect(s) an emergency generator to the class IE buses that are normally served by that emergency generator are considered to be part of the emergency generator train.
41 42 43	Emergency generators that are not safety grade, or that serve a backup role only (e.g., an alternate AC power source), are not included in the performance reporting.

Train Determination

- 2 The number of emergency AC power system trains for a unit is equal to the number of class 1E
- 3 emergency generators that are available to power safe-shutdown loads in the event of a loss of
- 4 off-site power for that unit. There are three typical configurations for EDGs at a multi-unit
- 5 station:

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- 1. EDGs dedicated to only one unit.
- 2. One or more EDGs are available to "swing" to either unit
- 3. All EDGs can supply all units

9 10

- 11 For configuration 1, the number of trains for a unit is equal to the number of EDGs dedicated to
- 12 the unit. For configuration 2, the number of trains for a unit is equal to the number of dedicated
- EDGs for that unit plus the number of "swing" EDGs available to that unit (i.e., The "swing"
- EDGs are included in the train count for each unit). For configuration 3, the number of trains is
- equal to the number of EDGs.

16 17

Clarifying Notes

- 18 The emergency diesel generators are not considered to be available during the following portions
- of periodic surveillance tests unless recovery from the test configuration during accident
- 20 conditions is virtually certain, as described in "Credit for operator recovery actions during
- 21 testing," can be satisfied; or the duration of the condition is less than fifteen minutes per train at
- 22 one time:

23

- Load-run testing
- 25 Barring

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An EDG is not considered to have failed due to any of the following events:

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- spurious operation of a trip that would be bypassed in a loss of offsite power event
- malfunction of equipment that is not required to operate during a loss of offsite power event (e.g., circuitry used to synchronize the EDG with off-site power sources)
- failure to start because a redundant portion of the starting system was intentionally disabled for test purposes, if followed by a successful start with the starting system in its normal
- 34 alignment

35 BWR High Pressure Injection Systems

- 36 (High Pressure Coolant Injection, High Pressure Core Spray, and Feedwater Coolant
- 37 Injection)

- 39 Scope
- 40 Plants should monitor either the high-pressure coolant injection (HPCI), the high-pressure core
- spray (HPCS), or the feedwater coolant injection (FWCI) system, whichever is installed. The
- 42 turbine and governor (or motor-driven FWCI pumps), and associated piping and valves for

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1 2 3 4 5 6 7 8	line are not considered within the scope of the these systems. The emergency generator dedicated to providing AC power to the high-pressure core spray system is included in the scope of the HPCS. The HPCS system typically includes a "water leg" pump to prevent water hammer in the HPCS piping to the reactor vessel. The "water leg" pump and valves in the "water leg" pump flow path are ancillary components and are not included in the scope of the HPCS system. Train Determination
9 10 11 12 13 14 15	The HPCI and HPCS systems are considered single-train systems. The booster pump and other small pumps are ancillary components not used in determining the number of trains. The effect of these pumps on system performance is included in the system indicator to the extent their failure detracts from the ability of the system to perform its risk-significant function. For the FWCI system, the number of trains is determined by the number of feedwater pumps. The number of condensate and feedwater booster pumps are not used to determine the number of trains.
17 18 19	BWR Heat Removal Systems (Reactor Core Isolation Cooling or check:Isolation Condenser)
20	<u>Scope</u>
21 22 23 24 25	The Reactor Core Isolation Cooling (RCIC) system turbine, governor, and associated piping and valves for steam supply and exhaust are within the scope of the RCIC system. Valves in the feedwater line are not considered within the scope of the RCIC system. The Isolation Condenser and inlet valves are within the scope of Isolation Condenser system.
26	Train Determination
27 28 29 30 31	The RCIC system is considered a single-train system. The condensate and vacuum pumps are ancillary components not used in determining the number of trains. The effect of these pumps on RCIC performance is included in the system indicator to the extent that a component failure results in an inability of the system to perform its risk significant function
32	BWR Residual Heat Removal Systems
33	<u>Scope</u>
34 35 36 37	The functions monitored for the BWR residual heat removal (RHR) system are the risk-significant functions. The pumps, heat exchangers, and associated piping and valves for those functions are included in the scope of the RHR system.
38	Train Determination
39 40	The number of trains in the RHR system is determined by the number of parallel RHR heat exchangers.

PWR High Pressure Safety Injection Systems

Scope

The scope includes the pumps and associated piping and valves from both the refueling water storage tank and from the containment sump to the pumps, and from the pumps into the reactor coolant system piping. For plants where the high-pressure injection pump takes suction from the residual heat removal pumps, the residual heat removal pump discharge header isolation valve to the HPSI pump suction is included in the scope of HPSI system. Some components may be included in the scope of more than one train. For example, cold-leg injection lines may be fed from a common header that is supplied by both HPSI trains. In these cases, the effects of testing or component failures in an injection line should be reported in both trains.

Train Determination

In general, the number of HPSI system trains is defined by the number of high head injection paths that provide cold-leg and/or hot-leg injection capability, as applicable.

For Babcock and Wilcox (B&W) reactors, the design features centrifugal pumps used for high pressure injection (about 2,500 psig) and no hot-leg injection path. Recirculation from the containment sump requires operation of pumps in the residual heat removal system. They are typically a two-train system, with an installed spare pump (depending on plant-specific design) that can be aligned to either train.

For two-loop Westinghouse plants, the pumps operate at a lower pressure (about 1600 psig) and there may be a hot-leg injection path in addition to a cold-leg injection path (both are included as a part of the train).

For Combustion Engineering (CE) plants, the design features three centrifugal pumps that operate at intermediate pressure (about 1300 psig) and provide flow to two cold-leg injection paths or two hot-leg injection paths. In most designs, the HPSI pumps take suction directly from the containment sump for recirculation. In these cases, the sump suction valves are included within the scope of the HPSI system. This is a two-train system (two trains of combined cold-leg and hot-leg injection capability). One of the three pumps is typically an installed spare that can be aligned to either train or only to one of the trains (depending on plant-specific design).

For Westinghouse three-loop plants, the design features three centrifugal pumps that operate at high pressure (about 2500 psig), a cold-leg injection path through the BIT (with two trains of redundant valves), an alternate cold-leg injection path, and two hot-leg injection paths. One of the pumps is considered an installed spare. Recirculation is provided by taking suction from the RHR pump discharges. A train consists of a pump, the pump suction valves and boron injection tank (BIT) injection line valves electrically associated with the pump, and the associated hot-leg injection path. The alternate cold-leg injection path is required for recirculation, and should be

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included in the train with which its isolation valve is electrically associated. This represents a two-train HPSI system.

For Four-loop Westinghouse plants, the design features two centrifugal pumps that operate at high pressure (about 2500 psig), two centrifugal pumps that operate at an intermediate pressure (about 1600 psig), a BIT injection path (with two trains of injection valves), a cold-leg safety injection path, and two hot-leg injection paths. Recirculation is provided by taking suction from the RHR pump discharges. Each of two high pressure trains is comprised of a high pressure centrifugal pump, the pump suction valves and BIT valves that are electrically associated with the pump. Each of two intermediate pressure trains is comprised of the safety injection pump, the suction valves and the hot-leg injection valves electrically associated with the pump. The cold-leg safety injection path can be fed with either safety injection pump, thus it should be associated with both intermediate pressure trains. This HPSI system is considered a four-train system for monitoring purposes.

PWR Auxiliary Feedwater Systems

Scope

- The scope of the auxiliary feedwater (AFW) or emergency feedwater (EFW) systems includes the pumps and the components in the flow paths from both the condensate storage tank and the
- alternative water source (e.g., the service water system). Startup feedwater pumps are not
- included in the scope of this indicator.

Train Determination

The number of trains is determined primarily by the number of parallel pumps. For example, a system with three pumps is defined as a three-train system, whether it feeds two, three, or four injection lines, and regardless of the flow capacity of the pumps. Some components may be included in the scope of more than one train. For example, one set of flow regulating valves and isolation valves in a three-pump, two-steam generator system are included in the motor-driven pump train with which they are electrically associated, but they are also included (along with the redundant set of valves) in the turbine-driven pump train. In these instances, the effects of testing or failure of the valves should be reported in both affected trains. Similarly, when two trains provide flow to a common header, the effect of isolation or flow regulating valve failures in paths connected to the header should be considered in both trains.

PWR Residual Heat Removal System

Scope

The functions monitored for the PWR residual heat removal (RHR) system are those that are required to be available when the reactor is critical. These typically include low-pressure injection and the post-accident recirculation mode used to cool and recirculate water from the containment sump following depletion of RWST inventory. The pumps, heat exchangers, and associated piping and valves for those functions are included in the scope of the RHR system.

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1 <u>Train Determination</u>

- 2 The number of trains in the RHR system is determined by the number of parallel RHR heat
- 3 exchangers. Some components are used to provide more than one function of RHR. If a
- 4 component cannot perform as designed, rendering its associated train incapable of meeting one
- of the risk-significant functions, then the train is considered to be failed. Unavailable hours
- 6 would be reported as a result of the component failure.